Design and Construction of a Fast Ion Loss Faraday Cup Array Diagnostic for JET
Design and Construction of a Fast Ion Loss Faraday Cup Array Diagnostic for JET

D. S. Darrow¹, S. Bäumel², F. E. Cecil³, V. Kiptily⁴, R. Ellis¹, L. Pedrick⁴, A. Werner², and JET-EFDA Contributors*
“This document is intended for publication in the open literature. It is made available on the understanding that it may not be further circulated and extracts or references may not be published prior to publication of the original when applicable, or without the consent of the Publications Officer, EFDA, Culham Science Centre, Abingdon, Oxon, OX14 3DB, UK.”

“Enquiries about Copyright and reproduction should be addressed to the Publications Officer, EFDA, Culham Science Centre, Abingdon, Oxon, OX14 3DB, UK.”
ABSTRACT
A thin foil Faraday cup array is being built to measure the loss of 3.5 MeV alpha particles and MeV Ion Cyclotron Heating (ICH) tail ions on JET. It will consist of nine detectors spread over five different poloidal locations and three radial positions. They will measure the poloidal distribution and radial scrape off of the losses. The detectors will be comprised of four layers of thin (2.5 micron) Ni foil, giving some resolution of the lost particle energy distribution as different ranges of energies will stop in different layers of the detector. One detector will utilize eight thinner (1.0 micron) foils to obtain a better-resolved energy distribution. These detectors will accept particles incident up to 45° from the normal to the foils.

1. INTRODUCTION
Magnetically confined fusion plasmas of the present and future rely on good confinement of energetic ions, e.g. ion cyclotron heating (ICH) tail ions or fusion-produced alpha particles, to maintain efficient heating. Conversely, poor confinement of the fast ions would not only impede heating, but could also damage the first wall surrounding the plasma. Measurement of fast ion losses allows determination of which plasma conditions promote or impede good fast ion confinement, and also can provide information about processes internal to the plasma that have induced the losses. The Joint European Torus (JET) has substantial ICH capability, and may also conduct future experiments with deuterium-tritium (DT) plasmas that would generate 3.5 MeV alpha particles. Consequently, it is an ideal facility in which to install fast ion loss diagnostics. In addition, the design and construction of a fast ion loss diagnostic for JET will have application to the International Thermonuclear Experimental Reactor (ITER). In particular, a loss diagnostic for JET will have to operate at elevated vessel temperature (250 C) and in a challenging neutron/gamma radiation environment (if DT operation proceeds). Two projects are underway to implement fast ion loss diagnostics for JET in 2005, a Faraday cup array described here and a scintillator probe described in a companion paper.1 The system described here will replace a previously operating thin foil Faraday cup loss detector in JET.2,3

2. DESIGN GOALS
Interesting fast ion loss physics topics for JET include prompt orbit loss from optimized and reversed shear discharges, MHD induced loss, ICH tail ion loss, and ICH induced radial diffusion. For all of these, resolution of the loss versus poloidal position on the wall, versus minor radial position, and good resolution in time are desirable. The Faraday cup array design provides these characteristics, with five poloidal positions, three radial locations, and a time resolution of 1 ms (1 kHz sampling). The system, because of a logarithmic detection system, will also have a eight decades of dynamic range.
3. DETECTOR ARRANGEMENT

The design of the detector array has had to meet numerous constraints, including the ability of the supporting structure to withstand large electromagnetic forces due to halo currents during plasma disruptions. Carbon-carbon composite tiles will protect the detectors from plasma heat flux. The Faraday cups will be mounted in array at a single toroidal position, but extending poloidally from near the midplane to ~0.7 m below it, as shown in Fig. 1. The array is supported by a curved inconel I-beam which is attached to the vacuum vessel. Five “pylons” project from the I-beam toward the plasma and each pylon can contain up to three thin foil Faraday cup stacks. At the inner end of each pylon is a circular carbon-carbon composite tile to protect the detectors from plasma heat flux. The curved I-beam is mounted by a pin into its lower support and a doubly-hinged link at its upper end. This arrangement allows the beam to expand thermally at a rate different from that of the vacuum vessel without inducing additional stresses in the supporting structure. An exploded view of an individual inconel pylon is shown in Fig. 2. The top plate contains three arrays of holes to admit fast ions to the foil stack—one array for each detector location within the pylon. Each Faraday cup assembly will consist of alternating layers of 2.5 μm Ni foil and 2.5 μm phlogophite mica sheets. The mica sheets insulate between adjoining foils, and phlogophite was chosen because of its ability to withstand temperatures over 1000°C, the calculated worst-case temperature the foils might reach. The fast ion currents reaching each foil will be transmitted to wires at a terminal block adjoining each stack. Glidcop wires will carry the signals to plug assemblies that will connect to pre-existing signal receptacles mounted inside the JET vessel. The recesses in each pylon that will hold the foil stacks will be flame sprayed with alumina to prevent shorting the foils to the pylon body.

The spacing between pylons was chosen to be approximately twice the DT alpha particle gyroradius under normal conditions in order to minimize the blocking of orbits reaching a detector by adjoining detectors. The detectors were moved as close to the plasma as deemed prudent by the engineering staff: the front face of each protective tile is 5 mm farther from the plasma than is the poloidal limiter. The tiles are 25 mm thick, the thinnest considered feasible for the heat flux generated by the plasma.

Each pattern of apertures consists of 112 3 mm diameter holes, giving a total active area of 792 mm². The aperture hole patterns extend 31 mm along the top of the pylon in the radial direction and 67 mm toroidally. As a consequence of the tile setback noted above and the 45° inclination of each pylon (described below), the pattern centers are at 46, 74, and 102 mm behind the poloidal limiter. Each hole is 3 mm diameter in a 3 mm thick inconel plate, giving a large solid angle from which fast ion loss orbits are accepted. This choice of aperture aspect ratio was made to enhance the generally low signal levels and it has the associated consequence that the detectors have very little selectivity in pitch angle.
The long axis of each pylon is inclined 45° above the normal to the surface of the I-beam at that pylon’s mounting point. This insures, in spite of the large aperture opening angle, that none of the foils have a direct line of sight into the plasma. This prevents possible photoemission from the foil surface from plasma-generated UV and soft X-rays, a signal which could be easily confused with fast ion deposition in the foils. Finally, each pylon is rotated in its mounting plane on the I-beam to turn the apertures toward the flux of co-going fast ions. Inclination in this direction is limited by a nearby beryllium evaporator: there should be no direct line of sight from the evaporator head onto the foil surfaces, so that a Be coating does not accumulate on the foil stack and change its energy calibration. The resultant inclination angles this constraint imposes are, starting from the top pylon and continuing down, 20°, 20°, 15°, 0°, and 0°.

For the bottom pylon, better energy resolution will be obtained by using eight 1.0 µm thick Ni foils. The aperture holes for this detector will be only 1.6 mm in diameter. In each pylon, the location closest to the plasma will always contain a foil stack. In the pylons at poloidal positions of 9° and 21°, all three positions will be populated with foil stacks in order to measure the radial scrape off profile of the fast ions.

4. ANTICIPATED SIGNAL LEVELS

The DT alpha particle signal levels expected for a range of plasma currents and toroidal field values are shown in Fig. 3 for the detectors closest to the plasma. These calculations have been made with the Lorentz orbit code [ref Felt], using actual plasma equilibria and fusion source rate profiles from several JET plasmas from its 1997 DT experiments. Signal levels are detectable over a reasonably wide range of conditions. Signal levels for the detector positions farthest from the plasma for each poloidal position and each assumed plasma are calculated to be roughly a factor of ten less than the signal levels shown in Figure 3, indicating the radial scrape off of alpha particles will be measurable under at least some conditions. Note that the loss rate of DD fusion products will be ~100 times smaller than that of DT alpha particles and, given the noise levels, is not expected to be measurable in most circumstances. On the other hand, losses of the energetic protons during D-3 He plasmas should be observable by virtue of the very large gyroradius.

Calculation of the expected ICH tail ion loss rate is a complex effort and has not been attempted in the process of designing these detectors. The loss currents could exceed the alpha particle currents by several orders of magnitude in some situations. The large dynamic range of the detection electronics should allow measurement of these losses.
5. SIGNAL TRANSMISSION AND DETECTION

Current from each Faraday foil is carried from outside the vessel to detection electronics ~100 m away. To minimize EMI effects on the signal, “superscreened” coaxial cables are used in this long cable run. Each foil is instrumented with a logarithmic amplifier capable of registering currents from 100 pA to 10 mA with a 1 kHz bandwidth. A total of 44 foils and channels of instrumentation are planned.

The entire diagnostic is intended to be operational beginning in spring 2005.

ACKNOWLEDGEMENTS

This work is supported by US Department of Energy contracts DE-AC02-76CH03073 & DE-FG03-95ER54303 and conducted under EFDA.

REFERENCES

[1]. S. Bäumel, et al., these proceedings.
[4]. Canberra MM20/75 and equivalent.
[5]. Analog Devices AD8304ARU
Figure 1: View of the Faraday cup detector array inside the JET vacuum vessel. The detectors are mounted on five “pylons” which are supported by a curved I-beam mounted to the vacuum vessel. Each of the pylons can contain up to three thin foil Faraday cup stacks.

Figure 2: Exploded view of a single pylon, showing the top plate with aperture holes, a stack of alternating Ni foils and mica insulators, terminal blocks, foil stack mounting recesses, backing plate and spring, and carbon-carbon composite protective tile with mounting hardware.
Figure 3: Calculated DT alphaparticle loss currents at the detector position closest to the plasma in each pylon. Calculations are based upon actual magnetic equilibria for JET DT discharges, with an alpha source profile of the form $S(p) = S_0 (1-p)^\alpha$, where $p$ is the normalized poloidal flux at a given position (0 on the magnetic axis and 1 at the separatrix or last closed surface), $\alpha$ is an exponent to match the experimentally observed profile, and $S_0$ is a constant. The line marked “Nominal noise level” is the noise level expected from a previous Faraday cup detector on JET, adjusted for the wider bandwidth of this system. The line marked “Optimistic noise level” assumes the data has been filtered to a bandwidth of 50 Hz and that common mode noise subtraction has been employed.

Figure 4: Calculated signal level for the detector position in each pylon farthest from the plasma. Cases and designations are as in Fig. 3.